AGGREGATION METHODS FOR NEARLY UNCOUPLED SYSTEMS



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OUTLINE

Intuitive overview of the Simon-Ando theory

Intuitive derivation and discussion of basic A/D

Analysis of errors in the basic A/D process

HISTORY

 H. Simon and A. Ando, Aggregation of variables in dynamic systems, Econometrica, Vol 29, pg. 111.

1975 - 1977 P. J. Courtois,

- Econometrica, Vol 43, pg. 691.
- Queueing And Computer System
 Applications, Academic Press.
- 1982 F. Chatelin and W. Miranker, Acceleration by aggregation of successive approximation methods, LAA, Vol 43, pg.17.
- 1984 McAllister, G. Stewart, W. Stewart, On a Rayleigh-Ritz refinement technique ... LAA, Vol 60, pg.1.



SHORT RUN EQUILIBRIUM

MID RUN RELATIVE EQUILIBRIUM



GOAL: Use short run info to estimate steady state









NEARLY UNCOUPLED MARKOV CHAINS

ASSUMPTIONS

- Large finite state space
- Homogeneous
- Irreducible
- Aperiodic

 Loosely connected clusters (say 3 of them) of closely connected states

NOTATION

Partitioned Transition Matrix

•
$$\mathbf{P} = \begin{bmatrix} \mathbf{P}_{11} & \mathbf{P}_{12} & \mathbf{P}_{13} \\ \mathbf{P}_{21} & \mathbf{P}_{22} & \mathbf{P}_{23} \\ \mathbf{P}_{31} & \mathbf{P}_{32} & \mathbf{P}_{33} \end{bmatrix}$$
 $\mathbf{e} = \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$
 $\mathbf{P}_{3} & \mathbf{0}$ $\mathbf{Pe} = \mathbf{e}$

After t Steps • $\frac{1}{4^{T}}(t) = \begin{bmatrix} \frac{1}{4^{T}}(t) & \frac{1}{4^{T}}(t) & \frac{1}{4^{T}}(t) \end{bmatrix} = \frac{1}{4^{T}}(0)\mathbf{P}^{t}$

Steady State

•
$$\frac{14^{T}(1)}{14^{T}} = \begin{bmatrix} 14^{T} & 14^{T} \\ 14^{T} & 14^{T} \end{bmatrix}$$

• $\frac{14^{T}}{14^{T}} = \frac{14^{T}}{14^{T}} \mathbf{P}$

SPECTRUM OF P



CENSORED CHAIN

OBSERVE PROCESS IN ONLY ONE CLUSTER



- $\mathbf{p}_{ij} = \mathbf{P}(i \text{ to } j \text{ directly})$
- $\mathbf{q}_{ij} = \mathbf{P}(\text{reenter cluster at } j^{\pm} \text{ leave from } \lambda)$

CENSORED PROBABILITY

CENSORED TRANSITION MATRIX

•
$$S = P_{11} + Q_{11}$$

QUESTION $\mathbf{Q}_{11} = ???$

-???

• $S_{11} = P_{11} + Q_{11}$

$$\mathbf{P} = \begin{bmatrix} \mathbf{P}_{11} & \mathbf{P}_{12} & \mathbf{P}_{13} \\ \mathbf{P}_{21} & \mathbf{P}_{22} & \mathbf{P}_{23} \\ \mathbf{P}_{31} & \mathbf{P}_{32} & \mathbf{P}_{33} \end{bmatrix}$$

 $\mathbf{Q}_{11} = \begin{bmatrix} \mathbf{P}_{12} & \mathbf{P}_{13} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{i} & \mathbf{P}_{22} & i & \mathbf{P}_{23} \\ i & \mathbf{P}_{32} & \mathbf{I}_{i} & \mathbf{P}_{33} \end{bmatrix} \begin{bmatrix} \mathbf{P}_{21} \\ \mathbf{P}_{31} \end{bmatrix}$

•
$$S_{11} = P_{11} + P_{1x} (I / P_1)^{1} P_{x1}$$

- Similarly for S₂₂ and S₃₃
- S//s are called stochastic complements

$$\mathbf{s}_{i}^{T}\mathbf{S}_{ii} = \mathbf{s}_{i}^{T}$$

• \mathbf{s}_{i}^{T} = steady state of i^{th} censored chain

BACK TO SIMON-ANDO



SIMON-ANDO (cont)



MID RUN RELATIVE EQUILIBRIUM

$\mathscr{U}_{4}^{T}(\mathfrak{k}) \mathscr{U}_{4}[\mathscr{W}_{1}(\mathfrak{k})\mathbf{S}_{1}^{T} \mathscr{W}_{2}(\mathfrak{k})\mathbf{S}_{2}^{T} \mathscr{W}_{3}(\mathfrak{k})\mathbf{S}_{3}^{T}]$



»(t) ! »;

LONG RUN STEADY STATE

 $\mathscr{V}_{4}^{T}(t) \neq \mathscr{V}_{4}^{T} = [\mathscr{W}_{1}\mathbf{S}_{1}^{T} \quad \mathscr{W}_{2}\mathbf{S}_{2}^{T} \quad \mathscr{W}_{3}\mathbf{S}_{3}^{T}]$

THE PROBLEM

GOAL

Estimate components in steady state

$$\mathscr{I}_{4}^{\mathcal{T}} = \begin{bmatrix} \mathscr{H}_{1} \mathbf{S}_{1}^{\mathcal{T}} & \mathscr{H}_{2} \mathbf{S}_{2}^{\mathcal{T}} & \mathscr{H}_{3} \mathbf{S}_{3}^{\mathcal{T}} \end{bmatrix}$$

WE KNOW

 s⁷/_i can be estimated by observing the short-run equibrium

REMAINING QUESTION

How can we estimate the coupling factors »_i?

A/D OPERATORS

AGGREGATION (RESTRICTION)

• **A**: $<^9$! $<^3$

DISAGGREGATION (PROLONGATION)

- **D** : $<^3 / <^9$
- **D**A = **I**

NATURAL CHOICES

$$\mathbf{A}_{9 \neq 3} = \begin{array}{c} 2 & & & 3 \\ \mathbf{e} & 0 & 0 \\ \mathbf{e} & 0 & \mathbf{5} \\ 0 & 0 & \mathbf{e} \end{array}$$

$$[\mathbf{p}_{1}^{T} \quad \mathbf{p}_{2}^{T} \quad \mathbf{p}_{3}^{T}] \mathbf{A} = [\mathbf{p}_{1}^{T} \mathbf{e} \quad \mathbf{p}_{2}^{T} \mathbf{e} \quad \mathbf{p}_{3}^{T} \mathbf{e}]$$

$$\mathbf{D}_{3 \neq 9} = \begin{array}{c} 2 & & & 3 \\ \mathbf{p}_{1}^{T} \quad \mathbf{p}_{2}^{T} \quad \mathbf{p}_{3}^{T}] \mathbf{A} = [\mathbf{p}_{1}^{T} \mathbf{e} \quad \mathbf{p}_{2}^{T} \mathbf{e} \quad \mathbf{p}_{3}^{T} \mathbf{e}]$$

$$\mathbf{D}_{3 \neq 9} = \begin{array}{c} 4 & 0 & & & \\ 0 & & & \mathbf{s}_{2}^{T} & 0 & 0 \\ 0 & & & & \mathbf{s}_{3}^{T} \end{array}$$

$$[\mathbf{w}_{1} \quad \mathbf{w}_{2} \quad \mathbf{w}_{3}] \mathbf{D} = [\mathbf{w}_{1} \mathbf{s}_{1}^{T} \quad \mathbf{w}_{2} \mathbf{s}_{2}^{T} \quad \mathbf{w}_{3} \mathbf{s}_{3}^{T}]$$

COUPLING MATRIX

DEFINITION

• C $(DPA)_{3 \pm 3} = {f s_{i} TP}_{ij} e^{\alpha}$

PROPERTIES

• **C** is irreducible and stochastic • For $\frac{1}{4}^{T} = [*_{1} \mathbf{s}_{1}^{T} *_{2} \mathbf{s}_{2}^{T} *_{3} \mathbf{s}_{3}^{T}]$ and $*^{T} = [*_{1} *_{2} *_{3}]$ it must be the case that $*^{T} \mathbf{C} = *^{T}$

CONCLUSION

If we can estimate the s⁷/_i's, then we can estimate the »ⁱ/_i's by computing the steady state vector of C.

BASIC A/D ALGORITHM

1. Somehow compute an estimate \mathbf{s}_{i}^{T} of each \mathbf{s}_{i}^{T}

VARIOUS POSSIBILITIES

Iterate until short-run approximate equilibrium is detected (until spectral components associated with small _ /s are annihilated)

 $\mathscr{H}^{\mathcal{T}}(\mathscr{I}) = \begin{bmatrix} \mathbf{c}_{1}^{\mathcal{T}} & \mathbf{c}_{2}^{\mathcal{T}} & \mathbf{c}_{3}^{\mathcal{T}} \end{bmatrix} \qquad \mathcal{B}_{i}^{\mathcal{T}} = \frac{\mathbf{c}_{i}^{\mathcal{T}}}{\mathbf{c}_{i}^{\mathcal{T}}\mathbf{e}}$

• Approximate each stochastic complement $\mathbf{S}_{ii} = \mathbf{P}_{ii} + \mathbf{P}_{ix} (\mathbf{I}_i \mathbf{P}_i)^{i} \mathbf{P}_{xi}$ with an irreducible $\mathbf{S}_{ii} = \mathbf{0}$. Then compute

 $\mathbf{\hat{s}}_{i}^{T}$ = normalized (left) Perron vector of $\mathbf{\hat{S}}_{ii}$

Question: How can $\mathbf{\hat{S}}_{ii}$ be obtained?

Answer: Melt mass of $P_{i\alpha}$ into P_{ii}

- **\hat{\mathbf{S}}_{ii} = \mathbf{P}_{ii} + \text{diagonal}**
- **\hat{S}_{ii} = P_{ii} + low rank update**
- **\hat{\mathbf{S}}_{ii} = \mathbf{P}_{ii} (i.e., ignore \mathbf{P}_{iz})**

A/D ALGORITHM (Cont)

2. Approximate the coupling matrix $\mathbf{C} = \begin{bmatrix} \mathbf{s}_{i}^{T} \mathbf{P}_{ij} \mathbf{e} \end{bmatrix}$ by computing

•
$$\mathbf{\hat{e}} = [\mathbf{\hat{s}}_{i}^{T}\mathbf{P}_{ij}\mathbf{\hat{e}}]$$

3. Estimate the coupling vector $\mathbf{w}^{T} = [\mathbf{w}_{1} \quad \mathbf{w}_{2} \quad \mathbf{w}_{3}]$ with the steady state vector of $\mathbf{\hat{e}}$

• Solve $b_{\beta}^{T} = b_{\beta}^{T} c$ for $b_{\beta}^{T} = [b_{1} \ b_{2} \ b_{3}]$

4. Approximate $\mathcal{U}_{4}^{T} = [\mathbf{w}_{1} \mathbf{s}_{1}^{T} \mathbf{w}_{2} \mathbf{s}_{2}^{T} \mathbf{w}_{3} \mathbf{s}_{3}^{T}]$ with

• $\mathscr{U}^{\mathcal{T}} = [\mathscr{D}_1 \mathscr{D}_1^{\mathcal{T}} \quad \mathscr{D}_2 \mathscr{D}_2^{\mathcal{T}} \quad \mathscr{D}_3 \mathscr{D}_3^{\mathcal{T}}]$



THE IDENTITY

•
$$\mathbf{S}_{i}^{T} = \frac{\frac{1}{4_{i}^{T}}}{\frac{1}{4_{i}^{T}}\mathbf{e}}$$

SUGGESTS ITERATING

• by using $\mathscr{B}^{T} = [\mathscr{P}_{1} \mathbf{s}_{1}^{T} \mathscr{P}_{2} \mathbf{s}_{2}^{T} \mathscr{P}_{3} \mathbf{s}_{3}^{T}]$ from 1^{st} A/D step to build 2^{nd} approximation of \mathbf{s}_{1}^{T}

BUT
$$\mathbf{\hat{s}}_{i}^{T} = \frac{\mathbf{\hat{y}}_{i}\mathbf{\hat{s}}_{i}^{T}}{\mathbf{\hat{y}}_{i}\mathbf{\hat{s}}_{i}^{T}\mathbf{e}} = \frac{\mathbf{\hat{y}}_{i}\mathbf{\hat{s}}_{i}^{T}}{\mathbf{\hat{y}}_{i}} = \mathbf{\hat{s}}_{i}^{T}$$

SO WE MUST ITERATE IN OTHER WAYS

- Restart iteration with $\mathcal{U}^{T}(0) \tilde{\mathcal{A}} \boxtimes^{T}$
 - A/D acts an accelerator to an underlying smoothing iteration (e.g., power method)
 - Dynamic re-aggregation
 - Use an A/D output ^M as input to different aggregation stratedgy

STANDARD A/D





C_{3*E*3}

DYNAMIC RE-AGGREGATION







DYNAMIC RE-AGGRE. (alt)







BASIC A/D ERRORS

INTERMEDIATE ERRORS $\mathbf{\hat{S}}_{ij} \mathbf{\mathcal{I}}_{ij} \mathbf{S}_{ij} = \mathbf{P}_{ij} + \mathbf{P}_{jx} (\mathbf{I}_{j} \mathbf{P}_{j})^{j} \mathbf{P}_{xj}$ • $\mathcal{C}_{i} = \|\mathbf{S}_{i}\|_{1}$ $\mathcal{C} = \max_{i} f \mathcal{C}_{i} g$ $\mathbf{\hat{s}}_{i}^{T}\mathbf{\hat{S}}_{ii} = \mathbf{\hat{s}}_{ii}^{T}$ • $\pm_i = \|\mathbf{s}_i^T \mathbf{s}_i^T\|_1$ $\pm = \max_i f \pm_i g$ $\hat{\mathbf{C}} = \begin{bmatrix} \mathbf{s}_{i}^{T} \mathbf{P}_{ij} \mathbf{e} \end{bmatrix} \frac{1}{4} \mathbf{C} = \begin{bmatrix} \mathbf{s}_{i}^{T} \mathbf{P}_{ij} \mathbf{e} \end{bmatrix}$ • $\mathbf{F} = \mathbf{C} \neq \mathbf{\hat{e}}$ $b_{\mu}^{T} \hat{\mathbf{e}} = b_{\mu}^{T}$ • $\mathbf{f}^{T} = \mathscr{Y}^{T} : \mathscr{Y}^{T}$ $\mathscr{B}^{\mathcal{T}} = \begin{bmatrix} \mathfrak{b}_1 \mathfrak{b}_1^{\mathcal{T}} & \mathfrak{b}_2 \mathfrak{b}_2^{\mathcal{T}} & \mathfrak{b}_3 \mathfrak{b}_3^{\mathcal{T}} \end{bmatrix}$

THE BIG ONE

$$\left\| \mathcal{U}_{i}^{\mathcal{T}} \right\|_{1} \cdot ???$$

BASIC A/D ERRORS



OLD ANALYSIS

MAXIMUM DEGREE OF COUPLING

•
$$^2 = 2 \max_{i} f k \mathbf{P}_{i} k_{1} g$$

COURTOIS (1977)

Theorem $\left\| \mathcal{U}_{4}^{T} \right\|_{1} = \mathcal{O}(2)$

Proof Entire third chapter of his book

DIFFICULT POINTS

- Unknown Order Constants
- Asymptotic Arguments
- For validity, ²must be "small" but it can't be determined how small "small" must be.
- Cumbersome Notation & Hard To Follow

DIFFERENT APPROACH

THE GROUP INVERSE

• $\mathbf{Q} = (\mathbf{I} \neq \mathbf{P})$ 2 multiplicative group

•
$$\mathbf{Q} = \mathbf{X}^{1} \begin{bmatrix} 0 & 0 \\ 0 & \mathbf{B} \end{bmatrix} \mathbf{X} \quad \mathbf{Q}^{\#} = \mathbf{X}^{1} \begin{bmatrix} 0 & 0 \\ 0 & \mathbf{B}^{1} \end{bmatrix} \mathbf{X}$$

AKA Kato's reduced resolvent at Z = 0

$$(\mathbf{Z} \neq \mathbf{Q})^{j + 1} = \frac{\mathbf{G}_{j + 1}}{\mathbf{Z}} + \mathbf{G}_0 + \mathbf{Z}\mathbf{G}_1 + \mathbf{Z}^2\mathbf{G}_2 + \ell\ell\ell$$
$$\mathbf{G}_0 = \frac{1}{2 \frac{1}{4}} \int_{C_0}^{I} \frac{(\mathbf{Z} \neq \mathbf{Q})^{j + 1}}{\mathbf{Z}} = \mathbf{Q}^{\#}$$

PERTURBED EIGENVECTORS

• Consider
$${}^{-T}\mathbf{P} = {}^{-T}$$
 and ${}^{GT}\mathbf{\hat{P}} = {}^{GT}$
• If $\mathbf{E} = \mathbf{P}$ / $\mathbf{\hat{P}}$ then ${}^{-T}$ / ${}^{GT} = {}^{GT}\mathbf{E}\mathbf{Q}^{\#}$

ERGODICITY COEFFICIENTS

APPROXIMATE $_{2}(P)$ WITH $_{\mathcal{E}}(P)$

- $\mathcal{E}(\mathbf{P}_1\mathbf{P}_2)$ · $\mathcal{E}(\mathbf{P}_1)\mathcal{E}(\mathbf{P}_2)$
- 0 · ¿(**P**) · 1
- $\mathcal{E}(\mathbf{P}) = 0$ if and only if $\mathbf{P} = \mathbf{e}^{1/4}$

NORMS ALONE DON'T WORK WELL

- $k\mathbf{P}k_1 > 1$ possibly
- $k\mathbf{P}k_2$, 1 possibly
- $k\mathbf{P}k_7 = 1$ for all **P**

A PARTICULAR

$$\mathcal{E}(\mathbf{P}) = \max_{i:j} \frac{1}{2} \sum_{k=1}^{n} j p_{ik} i p_{jk} j$$

PROPERTIES

- $(\mathbf{P}_1\mathbf{P}_2) \cdot \mathcal{Z}(\mathbf{P}_1)\mathcal{Z}(\mathbf{P}_2)$
- $0 \cdot \mathcal{L}(\mathbf{P}) \cdot 1$ (= 1 iff \mathscr{P} pair of \mathscr{P} rows)
- $\mathcal{L}(\mathbf{P}) = 0$ if and only if $\mathbf{P} = \mathbf{e} \, \mathcal{I}_{4}^{T}$
- $j_{32}(\mathbf{P})/\mathcal{O}(\mathbf{P})$ (Bauer, Deutch, Stoer, `69)
- $k\mathbf{FP} k_7 \cdot k\mathbf{F} k_7 c(\mathbf{P})$ whenever $\mathbf{Fe} = 0$

•
$$k\mathbf{F}(\mathbf{I} \neq \mathbf{P})^{\#} k_{7} \cdot \frac{k\mathbf{F} k_{7}}{1 \neq \mathcal{E}(\mathbf{P})}$$

• $\mathcal{L}(\mathbf{I} \neq \mathbf{P})^{\#} \cdot \frac{n}{\min_{\mathcal{I} \neq \mathcal{I}} f_{\mathcal{I} \neq \mathcal{I}}}$ (Seneta, `93)

ANALYSIS

LET

• $\mathbf{\hat{S}}_{ii} = \mathbf{P}_{ii} + \mathbf{M}_i$ where $k\mathbf{M}_i k_7 = k\mathbf{P}_{ix} k_7$ SO THAT

•
$$\mathcal{C}_i \land k\mathbf{S}_{ii} \not= \mathbf{S}_{ii} k_1 \cdot \mathbf{2} = 2 \max_i k \mathbf{P}_{ix} k_1$$

PROPOSITION

If $\mathbf{s}_{i}^{T}\mathbf{\hat{s}}_{ii} = \mathbf{s}_{i}^{T}$ and \mathbf{S}_{ii} is $n_{i} \in n_{i}$ then

•
$$\pm i = \mathbf{s}_{i}^{T} \mathbf{s}_{i}^{T} \mathbf{s}_{i}^{T} \cdot \mathbf{c}_{i} \mathbf{c}_{i} \mathbf{s}_{i}^{T} \mathbf{s}_{i}^{T} \cdot \mathbf{s}_{i}^{T} \mathbf{s}_{i}^{T} \cdot \mathbf{s}_{i}^{T} \mathbf{s}_{i}^{$$

SPECTRUM SPLIT



 $\underline{f} = \max_{i} f_{\pm i} \mathcal{G}_{i} \stackrel{2}{\gg} \max_{i} n_{i}$

COUPLING ERROR

PROPOSITION For $\mathbf{F} = \mathbf{C} \neq \mathbf{e} = \mathbf{f} \mathbf{s}_{i}^{T} \mathbf{P}_{ij} \mathbf{e}^{\pi} \neq \mathbf{f} \mathbf{s}_{i}^{T} \mathbf{P}_{ij} \mathbf{e}^{\pi}$ $\mathbf{F} \mathbf{k}_{1} \cdot \pm^{2} \leq \frac{2}{3} \max_{i} n_{i}$

PROPOSITION For $\mathfrak{B}^{T}\mathfrak{E} = \mathfrak{B}^{T}$ • $k\mathfrak{W}^{T} \mathfrak{B}^{T} k_{1} \cdot k\mathfrak{F}(\mathbf{I} \mathfrak{C})^{\#} k_{7} \cdot \frac{k\mathfrak{F} k_{7}}{1 \mathfrak{C}}$

BUT

- $\mathbf{C} = \mathbf{DPA}$ and $\mathcal{L}(\mathbf{D}) = \mathcal{L}(\mathbf{A}) = 1$
- $\mathcal{L}(\mathbf{C}) = \mathcal{L}(\mathbf{DPA}) \cdot \mathcal{L}(\mathbf{D})\mathcal{L}(\mathbf{P})\mathcal{L}(\mathbf{A}) = \mathcal{L}(\mathbf{P})$

THEREFORE

• $k \gg^{T} j \stackrel{h}{\gg}^{T} k_{1} \cdot \frac{\pm^{2}}{1 j \not{c}(\mathbf{P})} \stackrel{2}{\gg} \frac{2 \max_{i} n_{i}}{1 j \not{c}(\mathbf{P})}$

TOTAL ERROR

EXACT $\mathcal{I}_{4}^{T} = \begin{bmatrix} \mathbf{w}_{1} \mathbf{s}_{1}^{T} & \mathbf{w}_{2} \mathbf{s}_{2}^{T} & \mathbf{w}_{3} \mathbf{s}_{3}^{T} \end{bmatrix}$ **A/D APPROX** $\mathcal{I}_{4}^{T} = \begin{bmatrix} \mathbf{b}_{1} \mathbf{s}_{1}^{T} & \mathbf{b}_{2} \mathbf{s}_{2}^{T} & \mathbf{b}_{3} \mathbf{s}_{3}^{T} \end{bmatrix}$





THIS IS A COMPUTABLE ESTIMATE

All quantities in this estimate are directly available from P



SUMMARY

- The more uncoupled, the better A/D works
- Not good for closely coupled problems
- Can be iterated, but not in obvious ways
- Analysis is not easy for iterative cases